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I, Susan POTTS BA ACIS,

Director of RWS Group plc, of Europa House, Marsham Way, Gerrards Cross, Buckinghamshire, England declare;

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2. That the translator responsible for the attached translation is well acquainted with the German and English languages.
3. That the attached is, to the best of RWS Group plc knowledge and belief, a true translation into the English language of the specification in German filed with the application for a patent in the U.S.A. on  
under the number
4. That I believe that all statements made herein of my own knowledge are true and that all statements made on information and belief are true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the patent application in the United States of America or any patent issuing thereon.

A handwritten signature in black ink, appearing to read "SUSAN P OTTS".

For and on behalf of RWS Group plc

The 30th day of June 2001



## compensation of thermal optical effects

### Technical field

5 The invention relates to a method for compensating optical thermal effects in accordance with the preamble of Patent Claim 1, an optical unit for this purpose in accordance with the preamble of Patent Claim 4, and an optical arrangement in accordance with the preamble of  
10 Patent Claim 10.

### Prior art

15 If optical elements are heated, their optical properties (refractive index, external contour) are generally changed, and this entails variations in the phase front of a beam guided in such elements (thermal lens, thermal birefringence). Thermal optical effects are chiefly extremely disruptive in the case of optical  
20 high-performance oscillators, since they worsen the beam quality of the high-performance laser beam to be generated (beam deformation, stress birefringence, beam deflections etc.). The thermal lensing effect and the optical aberrations are caused by anisotropic  
25 temperature distribution in the optical medium.

An example for the elimination of thermal optical effects, in particular, continuously operating high-performance CO<sub>2</sub> laser resonators is given in the publication by A.V. Kudryashov entitled "Intracavity Laser Beam Control", SPIE Conf. on Laser Resonator II, San Jose, Calif., pages 32-40; 1999. The compensation is undertaken here actively by means of what is called adaptive optics. The adaptive optics is a mirror, whose  
30 surface contour can be adjusted, in the folded beam path inside the resonator. The adjustment is undertaken with the aid of electrically drivable piezoelectric ceramics. To control the drive, a small portion of the  
35 output radiation is coupled out, guided through a

diaphragm and passed onto a thermal sensor. Depending on the received radiant power, the individual "mirror elements" are then driven via a control circuit so as to produce a mirror deformation which compensates 5 surface deformations of the other optical components. An analogous adaptive adjustment of a mirror surface in a folded beam path in the resonator is described in L. Flath, J. An, J. Brase, C. Varrano, C.B. Dane, S. Fuchs, R. Hurd, M. Kartz, R. Sawvel; "Development of 10 Adaptive Resonator Techniques for High-Power Lasers", the publication relating to the conference entitled "Workshop on Adaptive Optics for Industry and Medicine", Durham (GB); page 163-168, 12-16 July 1999.

15 The deformation of the laser resonator mirror for compensation purposes is described in N. Kugler, A. Vazquez, H. Laabs, H. Weber, "High-Power Solid-State Laser with Birefringence Compensation and Adaptive Resonator Mirror"; publication relating to the 20 conference "Workshop on Adaptive Optics for Industry and Medicine", Durham (GB); page 149-154; 12-16 July 1999.

25 Instead of varying the surface curvatures of optical components, in particular of mirrors, under active control, it is also possible for lenses to be displaced along the resonator axis in the laser resonator in order to compensate thermal effects at the active element. Such arrangements are described in St. Jackel, 30 I. Moshe, R. Lavi; "High Performance Oscillators Employing Adaptive Optics Comprised of Discrete Elements"; SPIE Conf. On Laser Resonator II, San Jose, Calif., page 42-49; 12-16 July 1999.

35 It is likewise possible to have a combination of a plurality of elements in a laser resonator which can be controlled as to their optical action. Thus, in I. Moshe, S. Jackel; "Enhanced Correction of Thermo-Optical Aberrations in Laser Oscillators", SPIE Conf.

on Laser Resonator II, San Jose, Calif., page 181-186; 12-16 July 1999 use is made of a lens which can be adjusted under control as to its distance from the laser resonator mirror and which has one Faraday 5 rotator each upstream and downstream of the active medium.

DE-A 197 14 175 discloses a compensation of the thermal lens in the laser medium which is effective over the 10 entire range of pumping power. The compensation of the thermal lens was achieved by virtue of the fact that a portion of the pumping light itself was used in the case of a longitudinally pumped active medium with its varying power in order to create an appropriate optical 15 element which compensates the thermal lens in the active medium. This element was either a modified launch mirror or an additionally inserted element acting as a lens with a negative focal length (a positive one in the case of a negative thermal lens in the laser medium). It would also be possible to use a 20 gaseous or liquid medium, located in a suitable cuvette, as the element. In addition to the pumping optical radiation, it would also be possible to send a portion of the generated laser power through an appropriate element of the resonator for compensation 25 purposes.

The arrangement described in US-A 3 434 779 served the 30 purpose of keeping a laser power constant, this being achieved by using thermal optical effects.

Constancy is kept by using a nitrobenzene cell which widens a laser beam irradiated into it, doing so as a function of the radiant power. This widened beam then 35 strikes a diaphragm which passes only the central beam region.

The compensation of thermal lensing effects in the laser resonator is described in the publication by

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R. Koch entitled "Self-adaptive optical elements for compensation of thermal lensing effects in diode end-pumped solid state lasers - proposal and preliminary experiments"; Optics Communications 140 (15 July 1997), 5 pages 158-164. The compensation was performed by means of a resonator mirror whose mirror substrate absorbed the pumping radiation and had a large positive coefficient of thermal expansion. Specified as a further compensation option was an antireflection-coated plate which had a large negative thermal coefficient of the refractive index.

10 Further examples are described in US-A 5 386 427,  
15 US-A 5 751 750, US-A 3 662 281, US-A 3 609 584,  
US-A 3 577 098 and US-A 4 848 881.

#### **Object of the invention**

20 The object of the invention is to achieve, by contrast with the prior art, a substantially more effective compensation of the above-described optical changes caused by radial temperature gradients in optical components.

#### **25 Achievement of the object**

The above-named object is achieved by virtue of the fact that by contrast with the prior art, the various functions of absorption (heating by means of radiation absorption), radial thermal conduction (for generating a power-dependent temperature distribution) and thermal dispersion (for generating a thermal lens) are distributed over various, that is to say a plurality of elements with different material properties. By 30 contrast with the prior art, there is now no need for one and the same element to fulfill all functions.

35 By contrast with the prior art, the aim here is direct heat transfer by means of intimate contact between an

optical component and the compensation medium. The aim is preferably to achieve an approximately identical radial thermal distribution in the optical component and in the compensation medium.

5

Use may be made as compensation medium of materials which cannot transmit mechanical shear forces, or can transmit only negatively small ones. Such materials are liquids, gels and gases. However, it is also possible to use elastic media (solid bodies). However, in the case of solid bodies it is to be ensured that surfaces bearing against one another do so closely in optical terms, preferably being optically contacted. Optical surface effects should not arise in this case.

15

This type of compensation can be applied in the case of many optical components; however, they will preferably be used with lasers, in particular high-performance lasers, in which a good beam quality is desired.

20

Introduced into the beam path of an optical arrangement, which can be a laser oscillator or laser amplifier, for example, is an optical unit for compensating thermal optical effects in the beam path by means of optical components present therein. The optical unit located in the beam path has optical elements which have at least two different material properties and cooperate actively for the compensation, and on which, for the purposes of compensation, heating by means of radiation absorption, thermal conduction for generating a power-dependent temperature distribution, and thermal dispersion for generating a thermal lens can be distributed, preferably with a different effect.

35

One of the elements has an optical compensation space which is filled, in particular completely filled, with an optically transparent compensation medium. Optically transparent solid bodies are arranged as a further

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element with radiation absorption on both sides of the compensation space. The compensation medium makes such close thermal contact with the solid bodies arranged on both sides that good heat transfer is ensured from the

5 solid bodies to the compensation medium. The optical compensation space can now only be the compensation medium when a solid body or a solid gel is involved; however, it can also be a space which is to be filled with the compensation medium if a liquid or a flowable

10 gel is involved.

The compensation space is preferably designed in such a way that it extends perpendicular to the optical axis of the beam path. If the optical unit is used in a

15 laser resonator, the components of the oscillator or amplifier are generally of circular cylindrical design, and cooling takes place at the periphery. Consequently, the compensation space is also designed with radial symmetry relative to the axis of the beam path, and the

20 radial extent of the compensation space relative to the optical axis of the beam path is adapted to that of the neighboring solid bodies. It is preferred to select the radial dimensions of the compensation space and/or of the compensation medium to be identical to those of the

25 adjacent neighboring solid body.

The solid body immediately neighboring the compensation medium will preferably be kept in a cooling holder which preferably completely encompasses the entire envelope of the solid body in intimate thermal contact. This produces a space-saving design with good efficiency.

35 If a material which transmits no mechanical shear forces is used as compensation medium, it is preferably possible to provide an expansion space which is connected to the compensation space and into which the compensation medium can undertake volumetric equalization in the event of thermal loading. Such an

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expansion space will be used chiefly in the case of a liquid or flowable compensation medium. Given a compensation medium of small volume, even only a small gas bubble is sometimes sufficient. If solid, non-flowing compensation media are used, it is possible to dispense with an expansion space, since the thermal expansion is small. The small expansion still present then pushes tightly against the neighboring optical components.

10 As already indicated above, an optical arrangement with  
such an optical unit is preferably designed as a laser  
resonator or laser amplifier in order, for example, to  
generate high laser output powers with good beam  
15 quality. In this case, the active medium is subdivided  
into partial media. A compensation space filled with a  
compensation medium is arranged as an optical element  
between the partial media and as a further optical  
element of the optical unit, each partial medium acting  
20 as an optically transparent solid body of the unit.  
Here, as well, solid and flowable media can be used as  
compensation medium. A compensation space into which  
flowable media can be filled will then be provided for  
such media. For non-flowable media, the medium itself  
25 will be produced with the required spatial dimensions.

The advantages of the invention and its fields of application emerge from the following description.

### 30 Brief description of the drawings

Examples of the method according to the invention and of the subject matter according to the invention are explained below with the aid of the figures, in which:

35 figure 1 shows a diagrammatic illustration of a laser resonator as an optical arrangement with a compensating optical unit.

5 figure 2 shows a variant of the illustration in  
figure 1, an active laser medium being split  
here into component elements, and the optical  
compensation being undertaken immediately  
between these elements,

10 figure 3 shows a variant of the exemplary embodiments  
illustrated in figures 1 and 2, and

15 figure 4 shows a variant of the optical arrangement  
illustrated in figure 3, there being a  
plurality of optical compensation elements,  
however.

20 **15 Ways of implementing the invention**

25 The laser resonator 1, illustrated by way of example in  
figure 1, is designed as a symmetrical resonator with  
two parallel mirrors 3a and 3b. Arranged in the laser  
resonator 1 are a laser rod 5 as active medium, two  
lenses 7a and 7b and the optical unit 9 according to  
the invention. As indicated diagrammatically by the  
arrows 11a and 11b, the laser rod 5 is pumped optically  
in a transverse fashion. This pumping heats the laser  
rod 5 in its interior. It is cooled on its exterior.  
The result is the formation of a temperature gradient  
in the laser rod 5; what is termed a thermal lens has  
been formed. The refractive power of this thermal lens  
changes with the irradiated pumping energy and the  
generated laser radiation, which leads in turn to  
variations in the mode of oscillation of the laser  
resonator, and then further influences the generated  
radiant power and modes thereof. Such a behavior is  
extremely undesirable.

30  
35 In the laser resonator 1 sketched in figure 1, the two  
lenses 7a and 7b are used for the purpose of optimum  
superimposition of the thermal lens in the laser rod 5  
with that in the unit 9.

The unit 9 used for thermal compensation comprises here two laterally cooled, optically transparent cylindrical rods 13a and 13b and a narrow compensation space 15 with a compensation medium 16. The compensation space 15 extends at right angles to the optical axis 14 of the beam path produced by the laser rod 5. A liquid or a gel can be used as compensation medium. Use may be made as compensation materials of water, deuterated water or optical liquids and gels such as, for example, preferably for the visible spectral region OCF-446, OCF-452, OCF-463, OC-431 A-LVP, OC-440, OC-459, OC-462, OCK-433, OCK-451. These products are produced, for example, by the company Nye Optical Products. A further compensation material is a silicone "SYLGARD 182" from Dow Corning. Use will preferably be made of fully deuterated, chlorinated and fluorinated gels or liquids for the spectral region of longer wavelength adjoining the visible region. Of course, other liquids and gels can be used. It is also possible to use gases with suitable optical and thermal properties (refractive index, thermal dispersion). The advantages of liquids and gels are a very pronounced negative thermal dispersion ( $dn/dT$ ) and the absence of thermally induced birefringence, since pressure gradients caused by thermal expansion cannot arise. These compensation media do not transmit any mechanical shear forces. An expansion space 19 is provided for volumetric equalization when the compensation medium is thermally loaded.

The rods 13a and 13b as well as the compensation medium 16 are cooled externally by a holder 17. Glass or, even better, a birefringent crystal comes into consideration as rod material for avoiding thermally induced depolarization. A birefringent crystal as rod 13a or 13b is particularly advantageous whenever the laser rod 5 is likewise birefringent. The crystal optic axes are to be aligned with one another.

The medium 16 is now heated to a small extent by absorption of a small portion of the transmitting laser radiation (residual absorption), and to the other 5 extent by thermal conduction from the neighboring rods 13a and 13b into the medium 16. For their part, the rods are heated by absorption of a small portion of the laser radiation transradiating them. It would also be possible, in addition, to irradiate heat transversely 10 from a heat source. In order to produce a power-dependent lens suitable for compensation in the compensation medium 16, too, power-dependent temperature distribution must be set up therein. This requires that the thermal conduction must take place in 15 a predominantly transverse fashion from the material (transverse to the axis 14 of the beam propagation). Particularly in the case of compensation media which are narrow in the direction of beam propagation, predominant cooling over the end faces would have the 20 effect that a temperature distribution set up is influenced chiefly by the intensity distribution of the transmitted beam and only to a slight extent by the power thereof. This process is avoided in the unit 9 by arranging the compensating medium between rods 13a and 25 13b which are heated by a slight absorption of the transmitted laser beam and are radially cooled. The desired power-dependent temperature distribution is now produced by the processes of heating, cooling and thermal conduction in the rods 13a and 13b and in the 30 medium 16, and transmitted to the compensation medium 16 by thermal contact.

Instead of heating only the rods 13a and 13b, the 35 heating can be performed by a low absorption of radiation in the compensation medium 16. Irrespective of whether the heating is predominantly produced by absorption in the compensation medium 16 or in the rods 13a and 13b, the desired power-dependent lens is set up owing to the thermal contact of the compensation medium

16 with the neighboring rods 13a and 13b, and to the  
radial cooling of the rods 13a and 13b. By contrast  
with the prior art, the different functions of  
absorption (heating), radial thermal conduction (for  
5 generating a power-dependent temperature distribution)  
and thermal dispersion (for generating the thermal  
lens) are distributed here over various elements with  
different material properties, and need not all be  
fulfilled by one and the same element.

10

The strength of the lens produced and, if appropriate,  
the absorption can be optimized by mixing various  
materials (for example water and heavy water), and by  
selecting a suitable thickness  $d$  of the compensation  
15 space 15. By cooling the periphery of the rods 13a and  
13b with the aid of a holder 17 which encompasses them  
and which likewise cools the compensation medium 16  
externally, a power-dependent, radially decreasing  
temperature distribution is produced, which leads to a  
20 power-dependent lens because of the thermal dispersion  
of the compensation medium 16. The temperature  
distribution in the compensation medium 16 is  
approximately equal to that in the neighboring rods 13a  
and 13b because of the small dimension of the thickness  
25 of the compensation space 15.

The compensation medium 16 and the rods 13a and 13b  
preferably have the same refractive index. As a result  
30 of this, no Fresnel reflections occur at the interfaces  
between the rod end face and compensation medium 16,  
and a deformation based on the thermal expansion of the  
rods 13a and 13b does not lead to a lensing effect. The  
Fresnel reflections could certainly be suppressed by an  
35 antireflection coating, but this would entail making  
the unit 9 more expensive. The liquids and gels listed  
above are particularly suitable, because their  
refractive index can be set.

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The compensation space 15 can have two plane-parallel boundary surfaces (end faces of the rods 13a and 13b). However, it is also possible to undertake specific shaping such that even the higher aberrations, occurring in the laser rod 5, of the thermal lens can be adaptively compensated.

Given a sufficiently high thermal dispersion of the compensation medium 16, the thickness **d** of the compensation space 15 can be selected to be so small that no convection occurs. Specifically, convection would lead to striations. The convection can be avoided by selecting the viscosity suitably, and this is possible with the abovementioned materials by using suitable additives.

Data on the arrangement of the individual components are illustrated in **figure 1**. Here, the laser rod 5 is an Nd:YAG with a refractive index of  $n_L = 1.82$ , a length of  $L_L = 50$  mm and a diameter of 4 mm. One end face of the laser rod 5 has an axial distance of  $z - L_L/2n_L$  from one resonator mirror 3a.  $z$  is the distance between a resonator mirror 3a or 3b and the principal plane of the thermal lens. The magnitude of  $z$  influences the mode magnitude and the stability range of the laser resonator 1.  $z = 80$  mm. The focal length **F** of each lens 7a and 7b is 100 mm. The optical unit 9 has an axial length  $l_K$  of 20 mm. The rods 13a and 13b are made from glass with a refractive index of  $n_K = 1.5$  and a diameter of 4 mm. The thickness **d** of the compensation space 15 is smaller than 1 mm. OCF-446 has been used here as compensation medium 15.

If the thickness **d** is selected to be substantially larger, the viscosity of the compensation medium must also be increased, or a solid body must be used in order for there to be no convection accompanied by striations.

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A long path  $Z$  produces a larger mode diameter of the generated laser radiation, and thus a better beam quality, and this can be achieved by a lens placed additionally in the resonator. The distances  $Z$  between

5 the resonator mirror **3a** or **3b** and the principal plane  
of the thermal lens need not be selected to be equal on  
the left and right in the resonator 1. Then, the two  
resonator mirrors **3a** and **3b** need not be of planar  
design; they can also be arcuate. All that is involved  
10 here is one of many design variants, all of the optical  
components being variable.

The rods 13a and 13b can, of course, also have a cross section which is square, cuboid or of regular or irregular polygonal design. Again, the cross sectional contour can vary over the rod length. The rod length can be greater than the transverse rod dimension, but also substantially smaller than this (for example thin disks).

20 Instead of a solid rod 5 as active medium, it is also possible to use another amplifier medium (discharge tube [gas laser], liquid [dye laser], ...). The compensation of optical thermal effects is also not limited to laser resonators; it can also be used in the case of mechanisms based on nonlinear optical processes (frequency doubling, parametric amplification and oscillation, ...).

30 A further design variant of a laser resonator 29 is  
illustrated in **figure 2**, a laser rod having been  
subdivided here into a plurality of small partial rods  
30a to 30d, between which compensation is then  
undertaken. By analogy with **figure 1**, a compensating  
35 optical unit 34a to 34c now comprises in each case the  
two neighboring optically transparent solid bodies,  
that is to say the partial rods 30a and 30b, 30b and  
30c, and 30c and 30d. The compensation medium 39 is  
then arranged between the end faces of the neighboring

partial rods. The partial rods 30a to 30d are provided externally with a cooler 31, which simultaneously cools the compensation medium 39 in the compensation units 34a to 34c with the aid of the holders 35 thereof. The 5 resonator mirrors are marked here with 37a and 37b.

Owing to the heating in the laser rods and to the lateral cooling, a power-dependent temperature distribution, and thus a power-dependent positive thermal lens are set up in the partial rods 30a to 30d. Owing to the thermal contact between the end faces of the thermal rods 30a to 30d, this temperature distribution in the partial rods 30a to 30d is transmitted to the compensation medium, marked here with 39. As a result, a negative thermal lens, which compensates the positive thermal lens of the partial rods 30a to 30c, is produced in the compensation spaces 41a to 41c by the compensation medium 39 located there. There is no need in the compensation medium either for absorption of the laser power or of the pumping radiation. However, it is also possible to incorporate controlled absorption of the pumping light or of the laser radiation in the compensating medium. To be specific, all media absorb as a rule.

25 Intrinsically birefringent material, such as Nd:YVO<sub>4</sub>,  
for example, is preferably used for the laser rods. In  
that case, disturbing thermally induced birefringence  
does not occur either in the partial rods 30a to 30c or  
30 in the compensation medium. The optical axis of the  
partial rods 30a to 30c is aligned at right angles to  
the resonator axis 43. In order to average out any  
possible asymmetry in the thermal lens caused by the  
anisotropy of the material of the partial rods 30a to  
35 30c, the partial rods are arranged such that the  
optical axes are twisted in each case by 90° relative  
to one another in neighboring partial rods. In  
addition, the polarization of the transmitted laser  
radiation can then likewise be rotated by 90° between

the individual partial rods 30a to 30c by suitable optical elements. The amplification of the laser radiation can be optimized in this way (anisotropy of the crystals). In addition, it would also be possible 5 as an alternative to design the end faces of the partial rods in an arcuate fashion. Quartz rotators must be used if no birefringence occurs.

10 It will be preferred here to design the thickness of the compensation spaces **41a** to **41c** to be under 1 mm (for example 0.5 mm to 1 mm). The length of the partial rods can be a few millimeters to a few centimeters in the case of a typical rod diameter of 4 mm.  $z$  will typically be selected between 20 mm and 100 mm.

15 What has been set forth above with reference to the  
heat transfer and the geometry for the rods 13a and 13b  
is also valid mutatis mutandis for the partial rods 30a  
to 30d.

20 Transverse pumping of the laser rod 5 or 30a to 30d is  
illustrated in **figures 1 and 2**. Of course, it is also  
possible to use longitudinal pumping or other exciting  
mechanisms (gas discharge, RF excitation, gas dynamic,  
25 electronic, electric excitation, electron gun, ...) of  
the laser medium.

A variant of the optical arrangements shown in figures 1 and 2 is illustrated in figures 3 and 4. The variants illustrated here are simpler in their mechanical design. They can be used both for flowable and for non-flowable compensation materials. An exemplary use of the non-flowable compensation materials is described below.

35 A laser resonator 47 similar to that in **figure 2** is shown in **figure 3**. However, the laser resonator 47 exhibits substantial differences by comparison with the laser resonator 29. Here, a solid body, preferably an

elastomeric material, specifically the two-component gel OCK-433 mentioned above is used, in the cured state, as a unit 49 compensating thermal effects.

5 A double laser rod 50a/50b is arranged as active medium in the laser resonator 47, the two rods 50a and 50b being separated from one another by the compensating unit 49. The compensating unit 49 has a compensating medium 51, here the cured OCK-433, which is surrounded  
10 by a transparent sleeve 53 in which one end region 54a or 54b of the two end regions of the two rods 50a and 50b is plugged in each case. The cured OCK-433 serves firstly as compensation medium, and secondly also as a (cured) adhesive which lends the overall arrangement a  
15 stable coherence. The sleeve 53 is fabricated from sapphire, for example. Sapphire is transparent and has a very good thermal conductivity. Since the laser rods 50a and 50b generally have a circular cross section, the sleeve 53 is also designed with a circular cross section. The end regions 55a and 55b, not plugged in  
20 the sleeve 53, of the laser rods 50a and 50b are held in a holder 57 in a similar way as the arrangement in figure 2. The two laser rods 50a and 50b as well as the sleeve 53 are situated inside a transparent tube 60, which is filled with a cooling liquid 59 and which is likewise held in the holder. The two laser rods 50a and 50b as well as the sleeve 53 are cooled at their envelope by the cooling liquid 59. As is indicated by  
25 the two arrows P, the two rods 50a and 50b are pumped transversely in optical terms. The two resonator mirrors 62a and 62b are arranged at right angles to the optical resonator axis 61 in a fashion distanced from the outer end faces 63a and 63b, respectively, of the rods.

35

A very good thermal contact between the rod end faces and the compensating medium 51 is important. If, for example, the two-component gel OCK-433 is used, this can be introduced while still liquid between the rod

end faces. The gel is subsequently cured, forming a good thermal contact.

5 If use is made of elastomeric compensation media, they can be pressed over the adjacent laser rods 50a and 50b by means of the holder.

10 If, instead of an elastomeric material, use were made of a material with a higher modulus of elasticity, it would be necessary for the end faces and the assigned surfaces of the medium to be produced in a fashion adapted to one another in such a way that no "air transition" remains; optical contact would have to be made between the two neighboring surfaces. As regards 15 heating (absorption), radial thermal conduction (for producing a power-dependant temperature distribution) and thermal dispersion (for producing a thermal lens), the same applies for this arrangement as for the arrangement previously described.

20

Figure 4 shows a further design variant, which is constructed in a way similar to that illustrated in figure 3. However, here the active medium is split into four rods 67a to 67d aligned with one another. The 25 optical axis of the laser rods 67a to 67d coincides with the optical axis 69 of the laser resonator 70. The two middle rods 67b and 67c are designed with the same length; likewise the two outer ones 67a and 67d. Each of the outer rods 67a and 67d is only half as long as 30 each of the two middle rods 67b and 67c. Also present are three compensating units 71a, 71b and 71d for compensating thermal optical effects which comprise a compensating medium 72 and a sleeve 73. The arrangement relating to the laser rod end faces is undertaken in a 35 way similar to the design in figure 3. Here, as well, the laser rods 67a to 67d and the sleeves 73 of the units 71a to 71c are cooled in a way similar to figure 3 by a liquid 76 flowing in a transparent tube 75. The holder 77 for the tube 75 and the laser rod

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arrangement - 67a to 67d with 71a to 71c - corresponds to the holder 57 shown in Figure 3.

If high laser output powers are to be generated, long laser rods are also generally selected. If split up into a plurality of laser rods by comparison with the arrangement in **figure 3** this produces a better thermal optical compensation. What held for the laser rods **30a** to **30c** holds for the laser rods **50a** and **50b** and **67a** to **67b**.

As a rule, as a consequence of thermal optical conditions, a laser rod generates a thermally induced birefringence in the case of which a lower refractive index is produced for the radially polarized radiation component than for the tangentially polarized one. The compensating solid medium is now selected in the above exemplary embodiments in such way that the reverse effect is produced in the event of heating.

20 As already mentioned at the beginning, instead of the solid two-component gel OCK-433 it is also possible to use a liquid as compensation medium in the optical arrangement illustrated in **figures 3** and **4**. A small gas bubble which does not disturb the beam path will then 25 preferably be provided for the purpose of volumetric equalization. However, it is also possible to dispense with the volumetric equalization.

30 If solids, that is to say non-flowable materials are used as compensation media, it is possible to dispense with the sleeve 53 or 73 if the compensation medium behaves inertly relative to the cooling liquid.